

Low-noise Magnetic Field Measurements using Copper Permalloy Fluxgate Cores

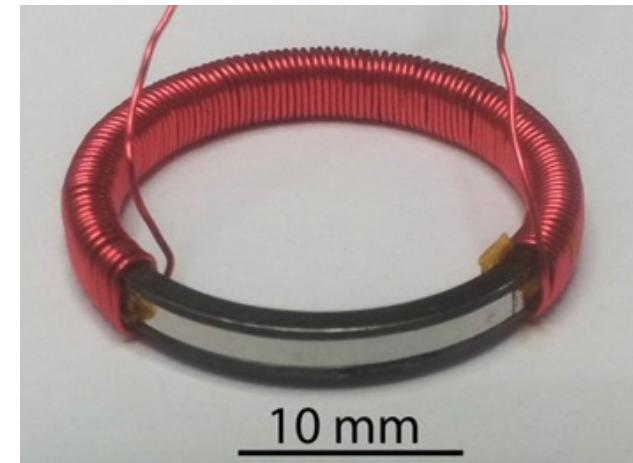
B. Barry Narod¹, David Miles²

¹ University of British Columbia

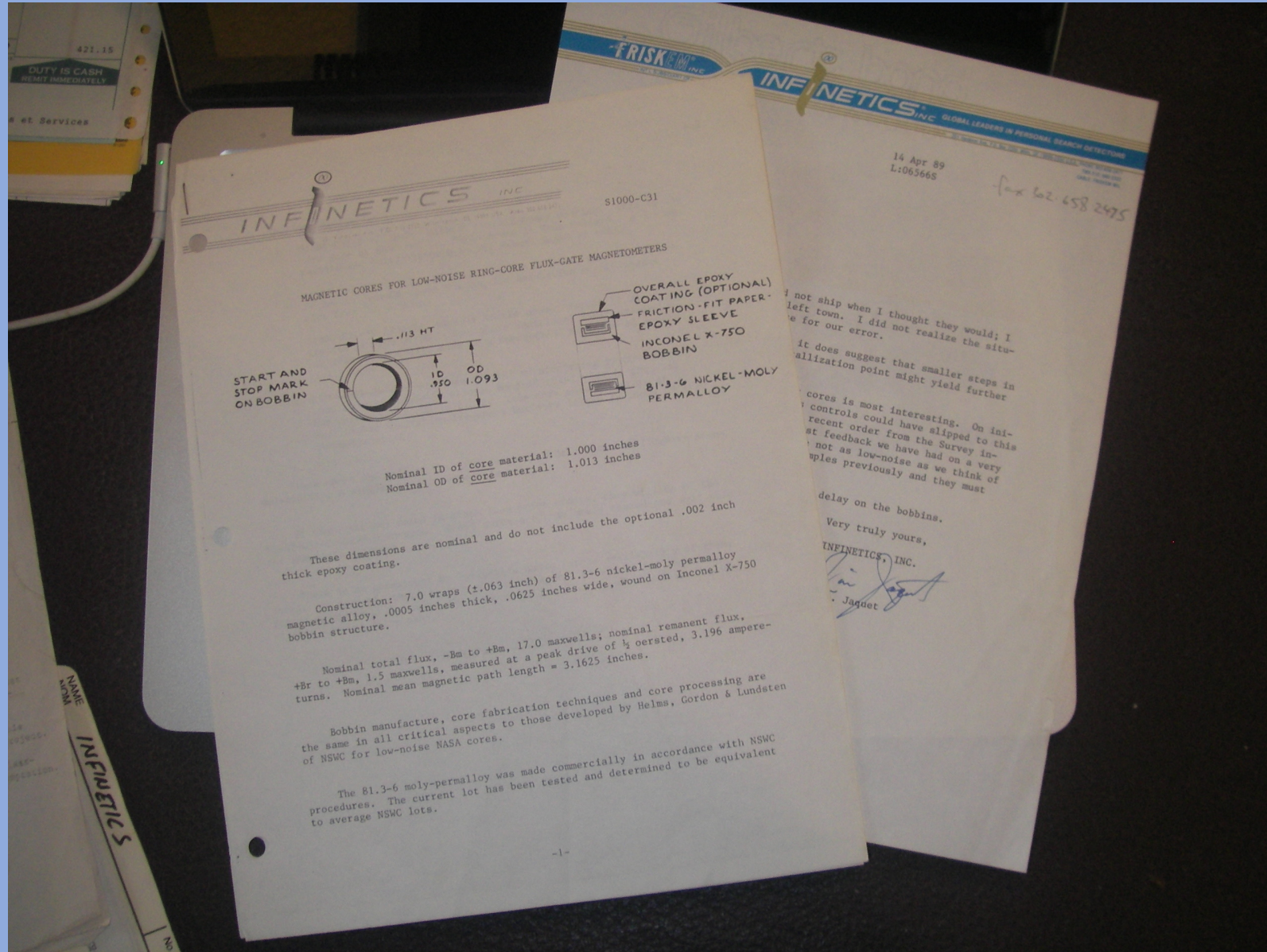
² University of Iowa

What is permalloy, and why do we care?

- Permalloy originated in 1923 and is a ferromagnetic alloy of Nickel and Iron. Additional alloying elements have been added to improve magnetic performance, molybdenum, chromium or copper.
- Our particular interest lie in Permalloy's use in low-noise fluxgate magnetometer sensors, for use in earth sciences, such as magnetotelluric surveys, magnetic observatories or in space physics.
- **At this time there is no long-term viable source of the lowest noise permalloy materials.**
- Our present examination of Copper Permalloys may be thought of as a continuation of a copper Permalloy study undertaken by Siemens & Halske, which terminated in 1937. These results include the first ever tests of copper alloys in fluxgate sensors.
- **Our new permalloys, new in both configurations and materials, should offer much improved performance compared with the now unavailable legacy devices.**

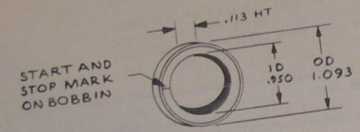


A bit of history about our favored Infinetics S1000 series ring cores



INFINETICS INC
S1000-C31

MAGNETIC CORES FOR LOW-NOISE RING-CORE FLUX-GATE MAGNETOMETERS



- OVERALL EPOXY COATING (OPTIONAL)
- FRICITION-FIT PAPER-EPOXY SLEEVE
- INCONEL X-750 BOBBIN
- 81.3-6 NICKEL-MOLY PERMALLOY

Nominal ID of core material: 1.000 inches
Nominal OD of core material: 1.013 inches

These dimensions are nominal and do not include the optional .002 inch thick epoxy coating.

Construction: 7.0 wraps (± 0.063 inch) of 81.3-6 nickel-moly permalloy magnetic alloy, .0005 inches thick, .0625 inches wide, wound on Inconel X-750 bobbin structure.

Nominal total flux, -Bm to +Bm, 17.0 maxwells; nominal remanent flux, +Br to +Bm, 1.5 maxwells, measured at a peak drive of $\frac{1}{2}$ oersted, 3.196 ampere-turns. Nominal mean magnetic path length = 3.1625 inches.

Bobbin manufacture, core fabrication techniques and core processing are the same in all critical aspects to those developed by Helms, Gordon & Lundsten of NSWC for low-noise NASA cores.

The 81.3-6 moly-permalloy was made commercially in accordance with NSWC procedures. The current lot has been tested and determined to be equivalent to average NSWC lots.

14 Apr 89
L:1063665

fax 602 658 2475

not ship when I thought they would; I left town. I did not realize the situation for our error.

It does suggest that smaller steps in realization point might yield further

cores is most interesting. On infrequent order could have slipped to this at feedback we have had on a very not as low-noise as we think of aples previously and they must

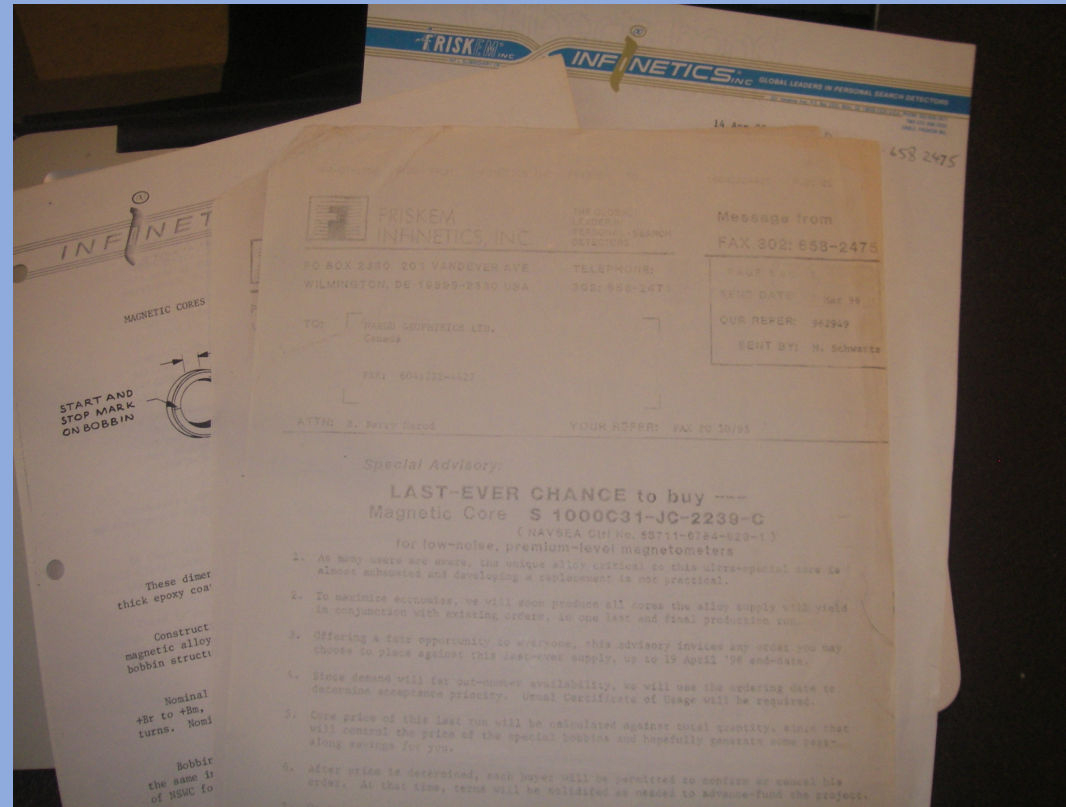
delay on the bobbins.

Very truly yours,

INFINETICS, INC.

Jagdet

A bit of history about our favored Infinetics S1000 series ring cores



Special Advisory

LAST-EVER CHANCE to buy ---

Magnetic Core S 1000C31-JC-2239-C ...

(NAVSEA Ctrl No. 53771-6784-629-1)

For low-noise, premium-level magnetometers...

“...one last and final production run...”

“...last-ever supply, up to 19 April, '96 end-date...” - M. Schwartz, 7 Mar 1996.

Two events now have moved us forward: 1) Figuring out the physics of magnetometer noise (2010)

Geosci. Instrum. Method. Data Syst., 3, 201–210, 2014
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doi:10.5194/gi-3-201-2014
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Instrumentation
Methods and
Data Systems

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The origin of noise and magnetic hysteresis in crystalline permalloy ring-core fluxgate sensors

B. B. Narod^{1,2}

¹Narod Geophysics Ltd., Vancouver, Canada

²Department of Earth, Ocean and Atmospheric Sciences, University of British Columbia, Vancouver, Canada

Correspondence to: B. B. Narod (bnarod@eos.ubc.ca)

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$$E_d \propto t^{-1/2} \times \alpha \times B_s^{3/2} \times K^{1/4}. \quad (8)$$

magnetocrystalline and magnetoelastic anisotropies and saturation induction, are all optimum in the Fe–Ni–Mo system.

In such polycrystalline permalloy fluxgate sensors, a sin-

A simplified domain energy model can then provide a predictive relation between ring-core magnetic properties and fluxgate sensor noise power. Four properties are predicted to

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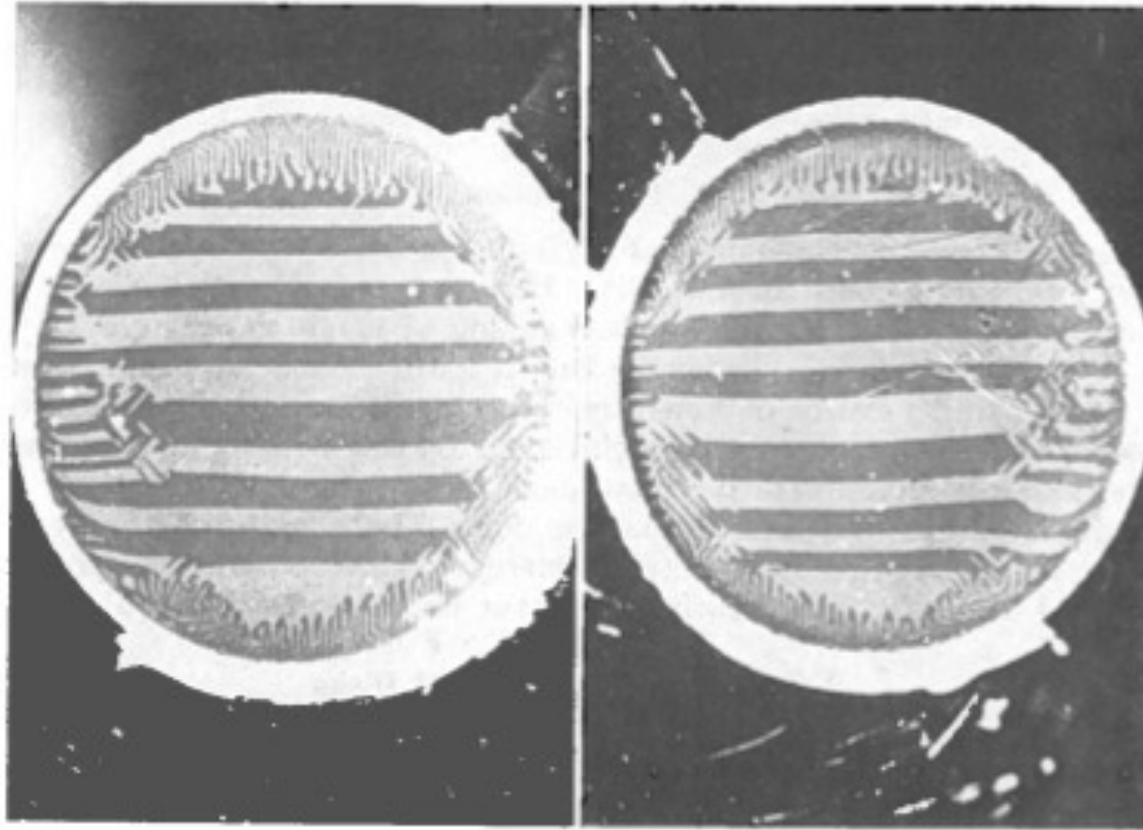
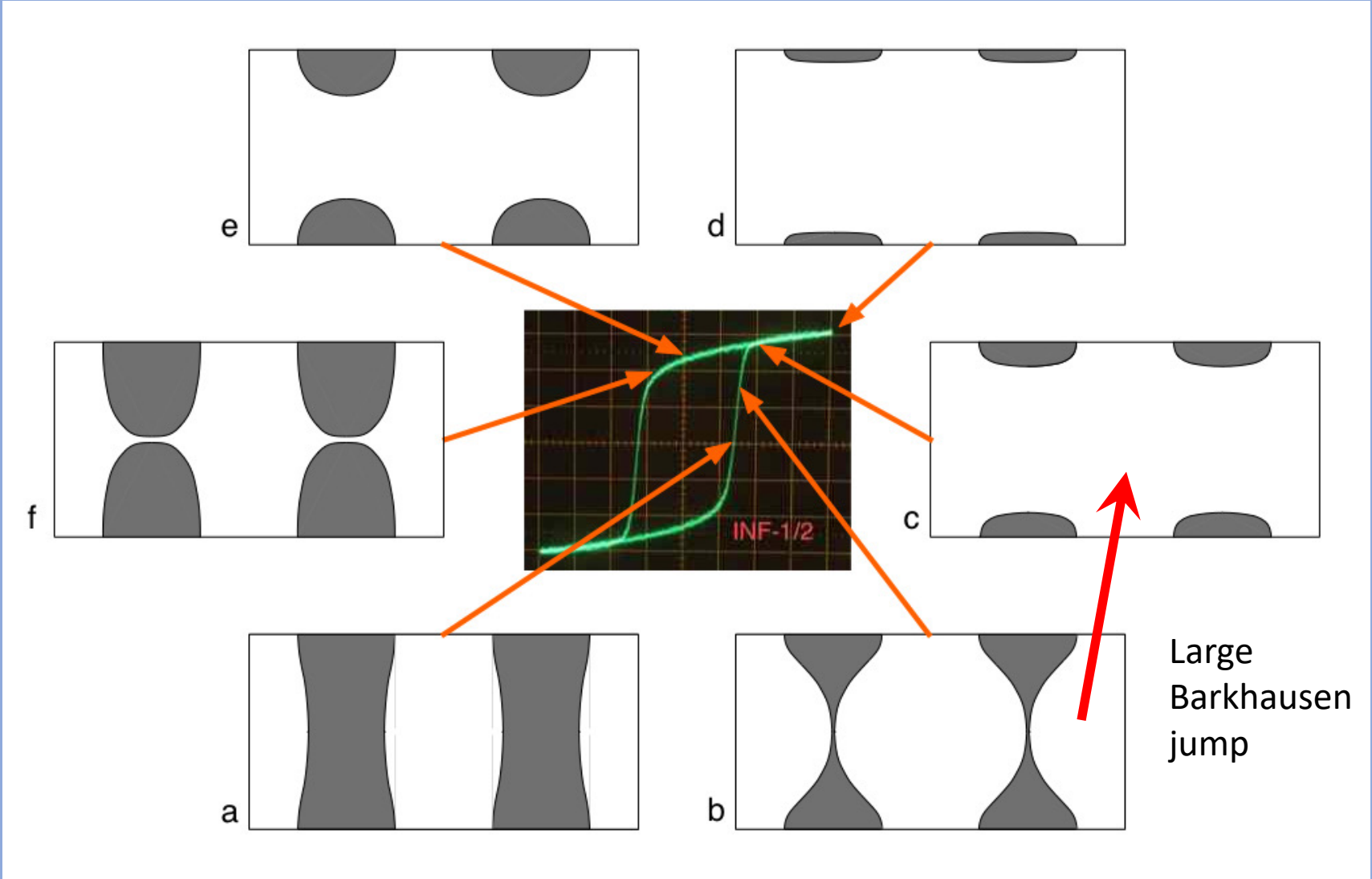


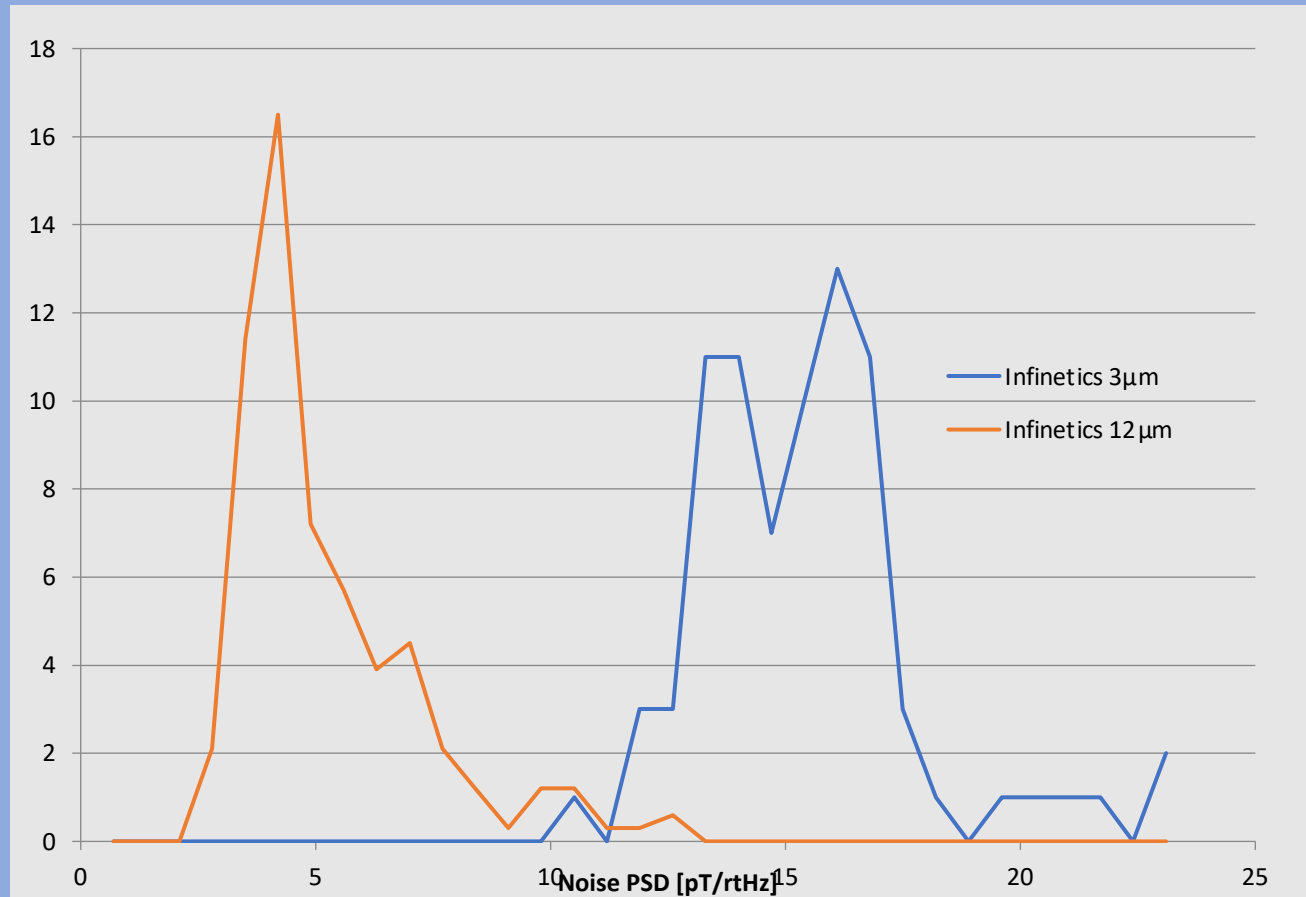
Fig. 1. Magnetic domain structures of the front and the back of a (110) single crystal disk with 38.7 at% Ni in Fe. The diameter of the sample is 7.5 mm; demagnetization in [001] direction

Stremme, 1974

The simplest grain:

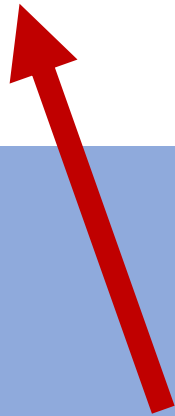
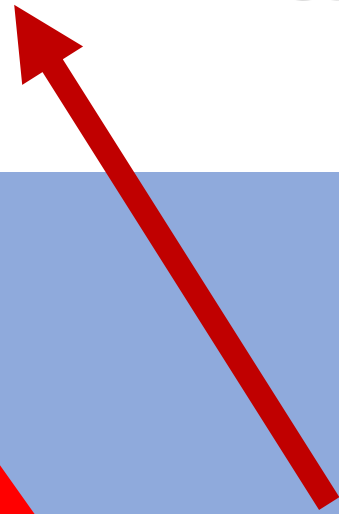
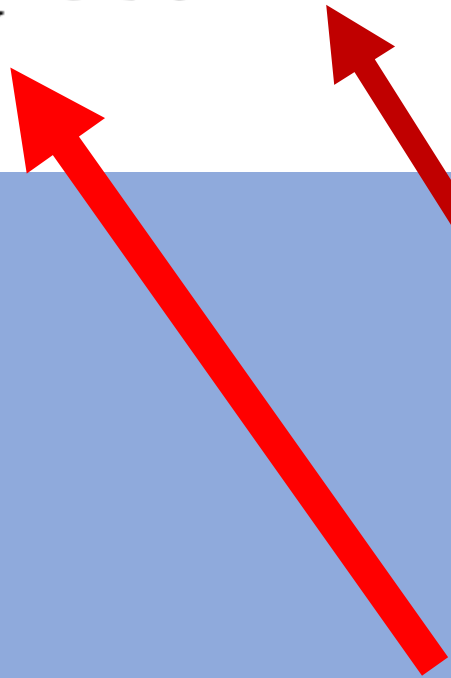
Actual stripe domains in a 7.5mm single crystal, viewed on a polished, carefully oriented cut face. Note the complex collection of closure domains at the grain perimeter.





Geometry matters! Noise increases with free surface area

$$E_d \propto t^{-1/2} \times \alpha \times B_s^{3/2} \times K^{1/4}.$$



Domain wall volumetric energy density

Foil thickness*

Crystalline alignment

Saturation moment

Total magnetic anisotropy

*or crystal size, whichever is smaller

Two events now have moved us forward: 2) Discovering the potential of Cu-permalloys (2007)

Überreicht vom Zentrallaboratorium des Wernerwerkes
der Siemens & Halske Aktiengesellschaft

Dr. Maxon Bitt. v. Schweidler

Über Eisen-Nickel-Kupfer-Legierungen hoher Anfangspermeabilität

Von

Otto v. Auwers und Hans Neumann

Mit 20 Bildern

Mitteilung aus dem Zentrallaboratorium
und der Abteilung für Elektrochemie des Wernerwerkes der Siemens & Halske A.-G.
und dem Forschungslaboratorium Siemensstadt

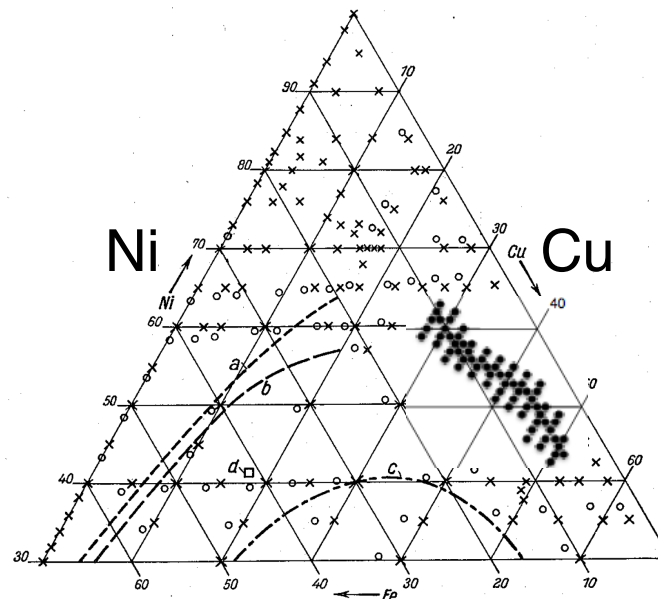
Eingegangen am 25. März 1935

History of copper permalloys

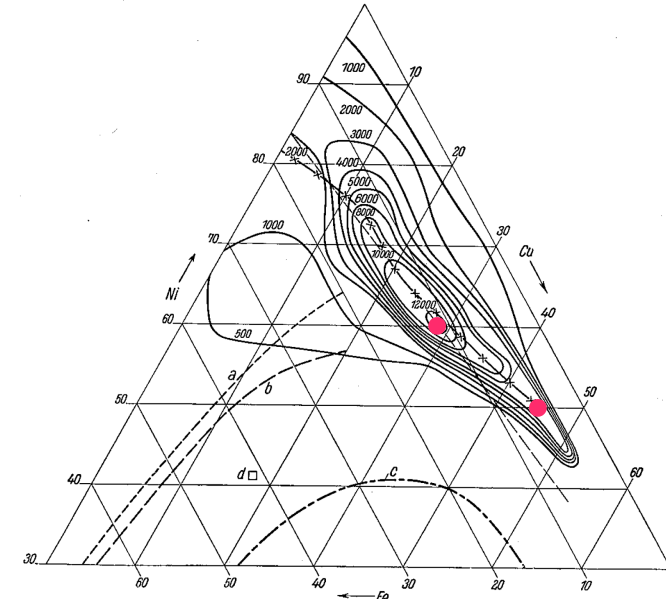
- These composition Figures show the 130 Copper alloys made for the 1935 Siemens and Halske study (circles and crosses), and the 50 Copper alloys made for our present study (left, larger dots).

- The right Figure shows the initial permeability contoured data from the original study.

- The red dots mark the end points of the range we have tested up to today, concentrated on the high permeability ridge.



Locations of alloys investigated in the FeNiCu-diagram

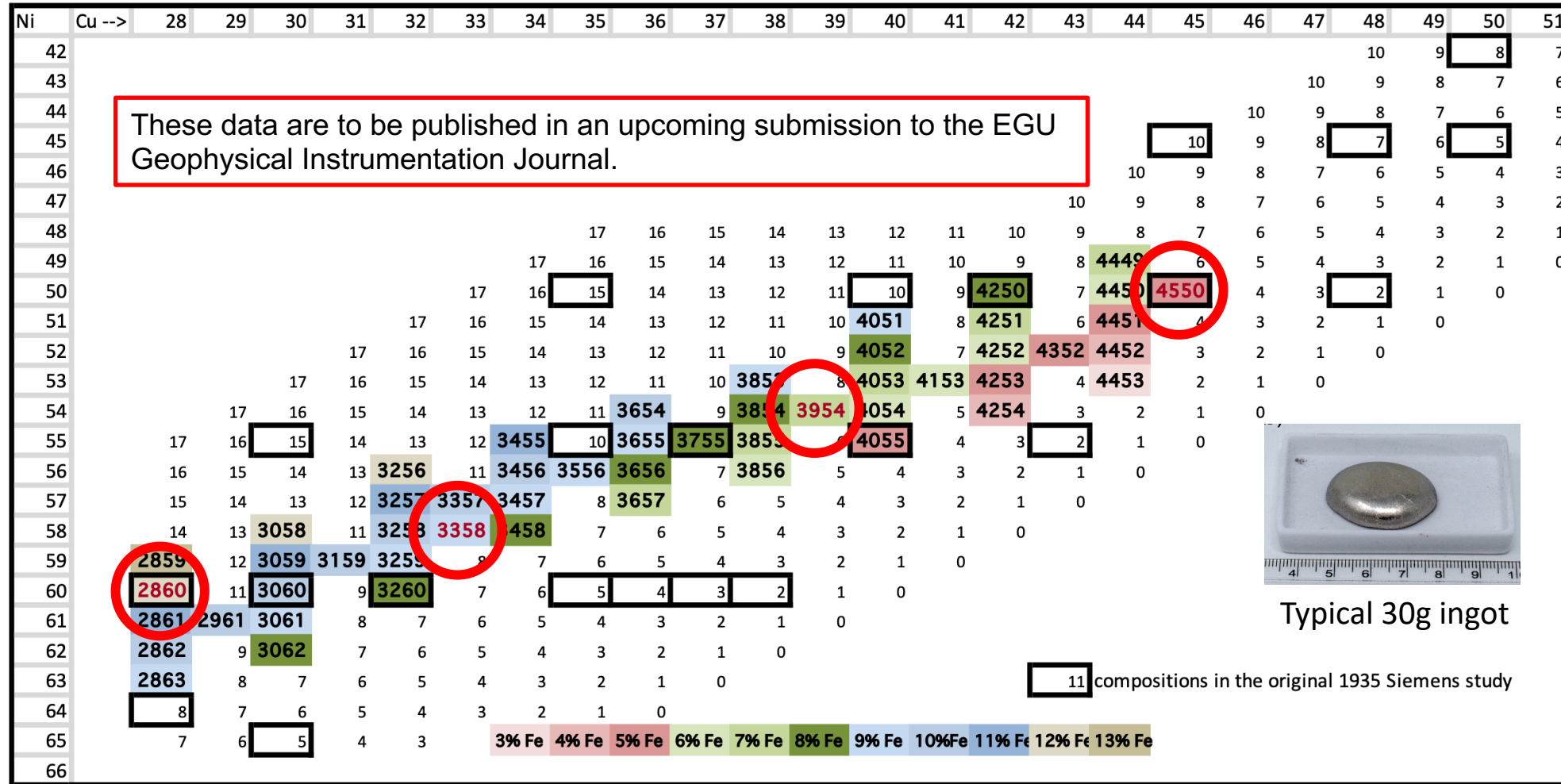


Lines of constant initial permeability - slow cooling

Original Figures from
Otto v Auwers and Hans Neumann, 1935
"Über Eisen-Nickel-Kupfer-Legierungen hoher Anfangspermeabilität"
(On Iron-Nickel-Copper Alloys of high initial permeability), Springer

Materials results - compositions

- Nickel content is plotted vertically, increasing down in 1% increments.
- Copper content is plotted horizontally, increasing to the right in 1% increments.
- Red circles/text mark compositions for more extensive testing.
- Small numbers are Iron contents, as are color codes.



Materials results - resistivity

- We present here resistivities as a function of Copper and Nickel contents.
- Red filled specimens are lower resistivity, and blue specimens are high resistivity.
- Resistivities for our Copper alloys are similar to those for more traditional Permalloys, with values increasing with both Cu and Ni contents. Higher resistivity reduces eddy current losses.

Resistivities at 20C, ohm-meters x 10⁻⁷

These data are to be published in an upcoming submission to the EGU Geophysical Instrumentation Journal.

Ni	Cu -->	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51					
42																						10	9	8	7					
43																						10	9	8	7	6				
44																						10	9	8	7	6	5			
45																						10	9	8	7	6	5	4		
46																						10	9	8	7	6	5	4	3	
47																						10	9	8	7	6	5	4	3	2
48									17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0				
49								17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0					
50							17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0						
51						17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0							
52					17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0								
53				17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0									
54			17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0										
55	17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0												
56	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0													
57	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0														
58	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0															
59	12	11	10	9	8	7	6	5	4	3	2	1	0																	
60	11	10	9	8	7	6	5	4	3	2	1	0																		
61	9	8	7	6	5	4	3	2	1	0																				
62	8	7	6	5	4	3	2	1	0																					
63	7	6	5	4	3	2	1	0																						
64	6	5	4	3	2	1	0																							
65	5	4	3	2	1	0																								
66	4	3	2	1	0																									

3.08
4.8
5.0
5.0

****** data not available
11 compositions in the original 1935 Siemens study
5.0 resistivity data from Delatorre et al, 2003

>2.80
>3.00
>3.20
>3.40
>3.60
>3.80
>4.00
>4.20
>4.40
>4.60
>4.80

Materials results – saturation induction

- Maximum saturation moment is at 28%Cu.
- Minimum saturation moment is at 44-45%Cu.
- Test conditions: +/- 1200 A/m 24Hz. Values are consistent with Auwers & Neumann (1935)
- Lower saturation moment reduces both power consumption and sensor noise.

Resistivities at 20C, ohm-meters x 10⁻⁷

These data are to be published in an upcoming submission to the EGU Geophysical Instrumentation Journal.

Ni	Cu -->	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51
42																						10	9	8	7
43																					10	9	8	7	6
44																				10	9	8	7	6	5
45																		10	9	8	7	6	5	4	3
46																		10	9	8	7	6	5	4	3
47																	10	9	8	7	6	5	4	3	2
48									17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1
49								17	16	15	14	13	12	11	10	9	8	3.62	6	5	4	3	2	1	0
50							17	16	15	14	13	12	11	10	9	**	7	3.93	4.30	4	3	2	1	5.0	
51						17	16	15	14	13	12	11	10	9	8	3.15	6	4.24	4	3	2	1	0		
52					17	16	15	14	13	12	11	10	9	8	7	**	4.04	4.54	4.55	3	2	1	0		
53				17	16	15	14	13	12	11	10	9	8	7	6	5	4	4.89	2	1	0				
54			17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0					
55		17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0						
56		16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0							
57		15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0								
58		14	13	3.08	11	3.31	3.22	3.57	7	6	5	4	3	2	1	0									
59		2.86	12	2.93	3.27	3.22	8	7	6	5	4	3	2	1	0										
60		3.08	11	3.21	9	3.66	7	6	5	4	3	2	1	0											
61		3.16	3.19	3.45	8	7	6	5	4	3	2	1	0	4.8											
62		3.24	9	3.55	7	6	5	4	3	2	1	0													
63		3.48	8	7	6	5	4	3	2	1	0														
64		8	7	6	5	4	3	2	1	0															
65		7	6	5	4	3																			
66																									

** data not available

11 compositions in the original 1935 Siemens study

5.0 resistivity data from Delatorre et al, 2003

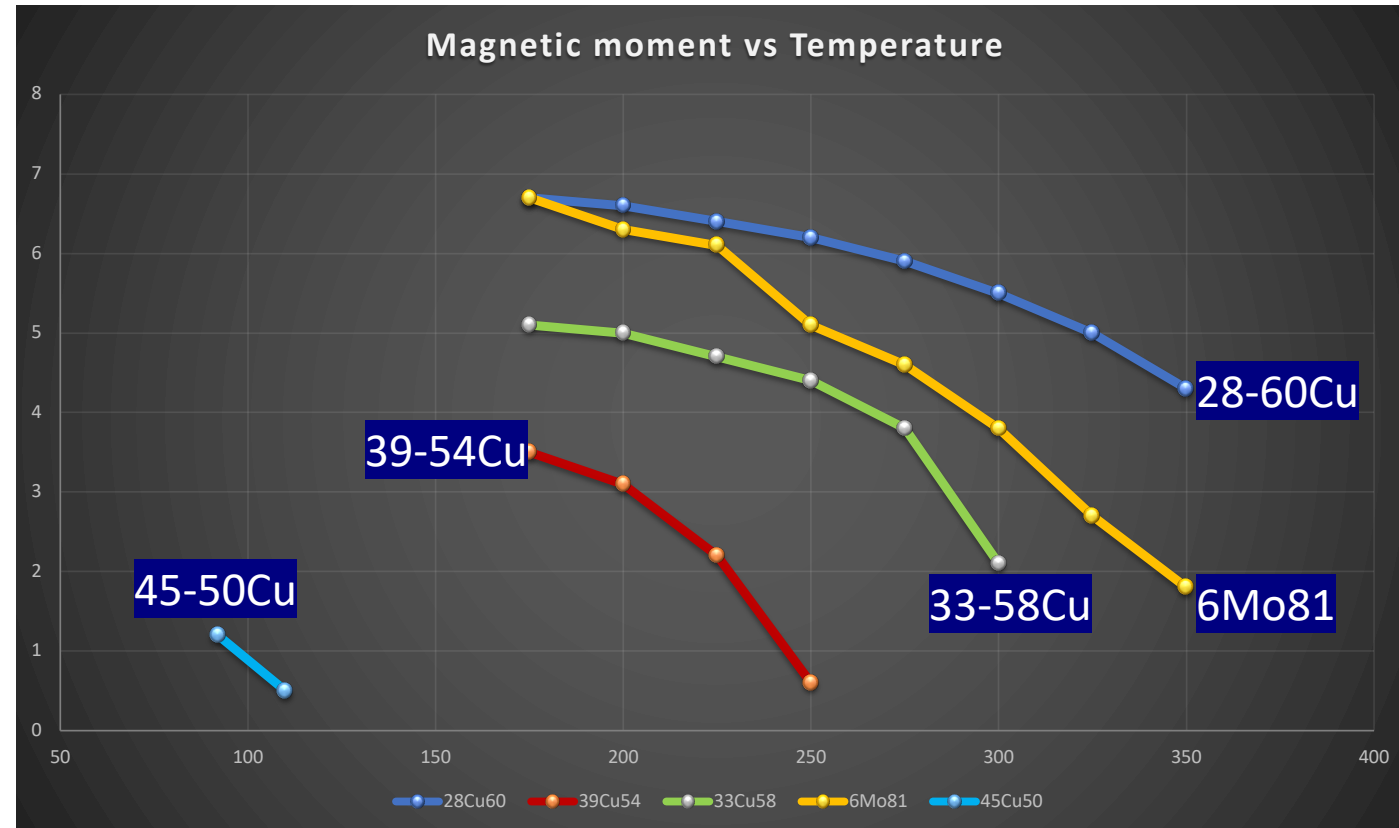
>2.80 >3.00 >3.20 >3.40 >3.60 >3.80 >4.00 >4.20 >4.40 >4.60 >4.80

Materials results – Curie temperature (preliminary)

- We present here Curie temperature data for our four studied Copper alloys, and for 6%Moly' Permalloy.

- Interpreted Tc's are:

- 6Mo81 360C
- 28-60Cu >360C
- 33-58Cu 310C
- 39-54Cu 250C
- 45-50Cu 100C



Materials results – Curie temperature

- Five specimens:
 - 28Cu60Ni
 - 33Cu58Ni
 - 39Cu54Ni
 - 44Cu51Ni
 - 45Cu50Ni
- 44Cu53Ni was paramagnetic.

Ni	Cu -->	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51		
42																							10	9	8	7	
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65																											
66																											

These data are to be published in an upcoming submission to the EGU Geophysical Instrumentation Journal.

<20 Curie temperature, C

11 compositions in the original 1935 Siemens study

Materials results – initial permeability

- Test conditions:
- +/- 0.4 A/m,
- 250Hz
- Cells outlined in red are a selection of local high values for permeability, and local low values for coercivity (next slide). Both are indicators for better noise performance (Musmann, 2010).

Ni	Cu -->	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51
42																						10	9	8	7
43																						10	9	8	7
44																						10	9	8	7
45																						10	9	8	7
46																						10	9	8	7
47																						10	9	8	7
48									17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1
49									17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1
50							17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0	
51						17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0		
52					17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0			
53				17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0				
54			17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0					
55		17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0						
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57	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0									
58	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0										
59	13	12	11	10	9	8	7	6	5	4	3	2	1	0											
60	12	11	10	9	8	7	6	5	4	3	2	1	0												
61	11	10	9	8	7	6	5	4	3	2	1	0													
62	10	9	8	7	6	5	4	3	2	1	0														
63	9	8	7	6	5	4	3	2	1	0															
64	8	7	6	5	4	3	2	1	0																
65	7	6	5	4	3	2	1	0																	
66																									

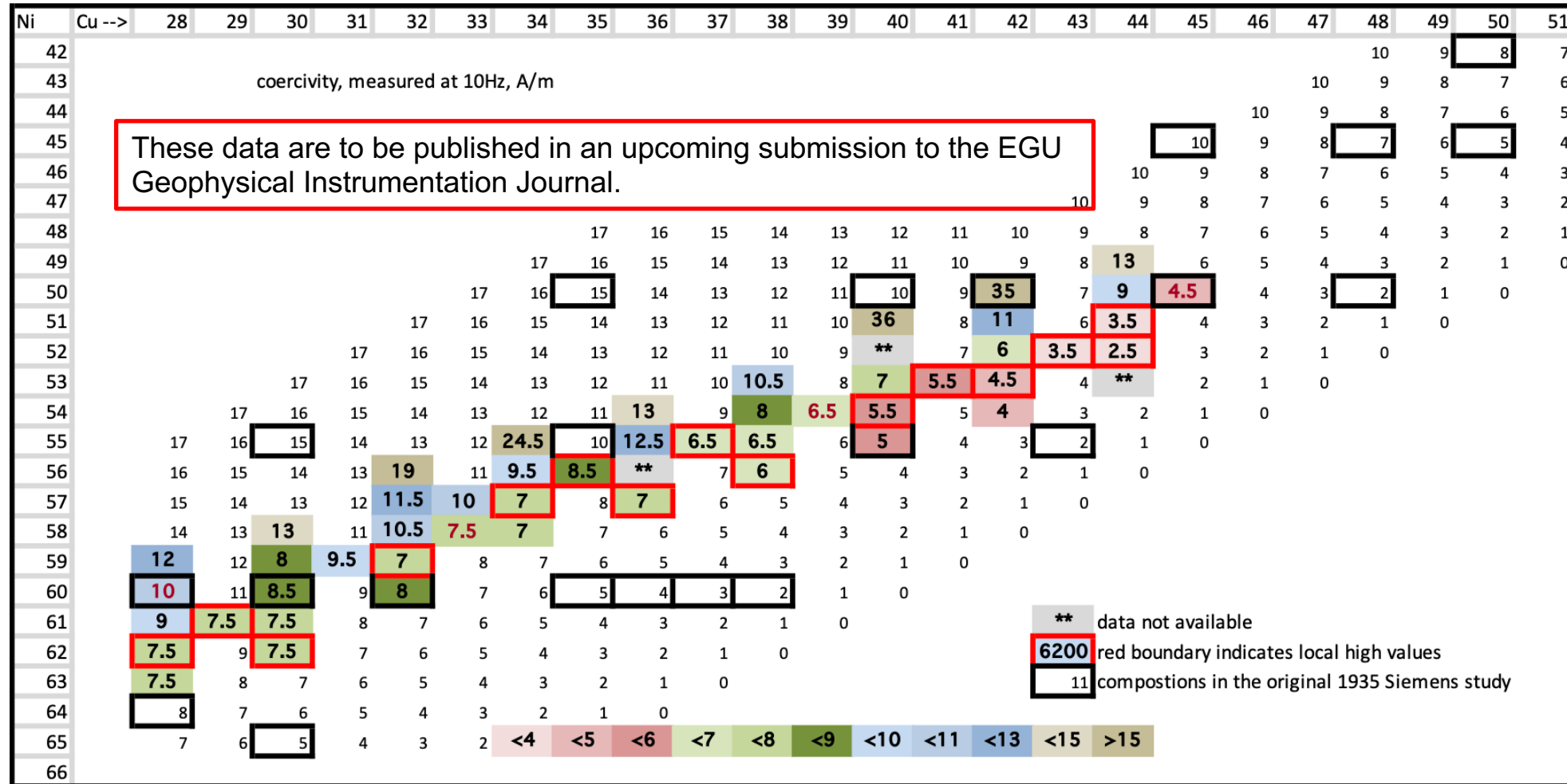
Initial relative permeability, G/Oe

These data are to be published in an upcoming submission to the EGU Geophysical Instrumentation Journal.

** data not available
 1400 initial relative permeability
 6200 red boundary indicates local high values
 11 compositions in the original 1935 Siemens study

Material results – 0Hz coercivity

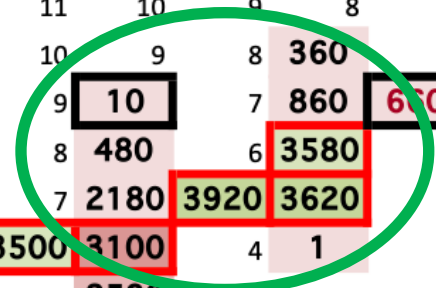
- Test conditions:
- +/- 50 A/m,
- 10Hz
- Cells outlined in red are a selection of local high values for permeability (previous slide), and local low values for coercivity.



Material results – initial permeability

Ni	Cu -->	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	
42																						10	9	8	7	
43																						10	9	8	7	6
44																				10	9	8	7	6	5	
45																			10	9	8	7	6	5	4	
46																			10	9	8	7	6	5	4	
47																			10	9	8	7	6	5	4	
48									17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	
49									17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	
50								17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0	
51					17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0				
52				17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0					
53			17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0						
54		17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0							
55	17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0								
56	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0									
57	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0										
58	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0											
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60	12	11	10	9	8	7	6	5	4	3	2	1	0													
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63	9	8	7	6	5	4	3	2	1	0																
64	8	7	6	5	4	3	2	1	0																	
65	7	6	5	4	3	2	1	0																		
66																										

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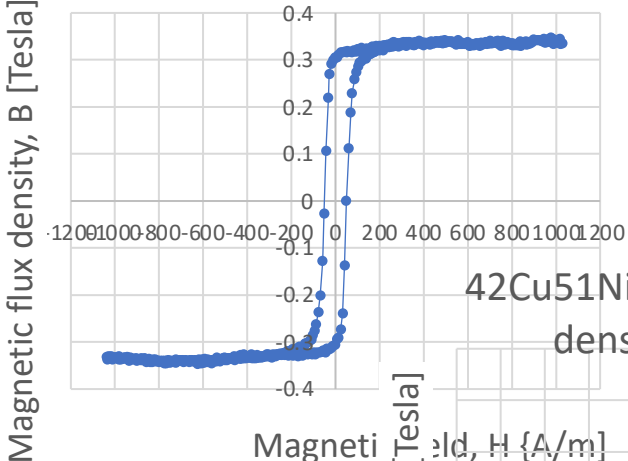


** data not available
 1400 initial relative permeability
 red boundary indicates local high values
 11 compositions in the original 1935 Siemens study

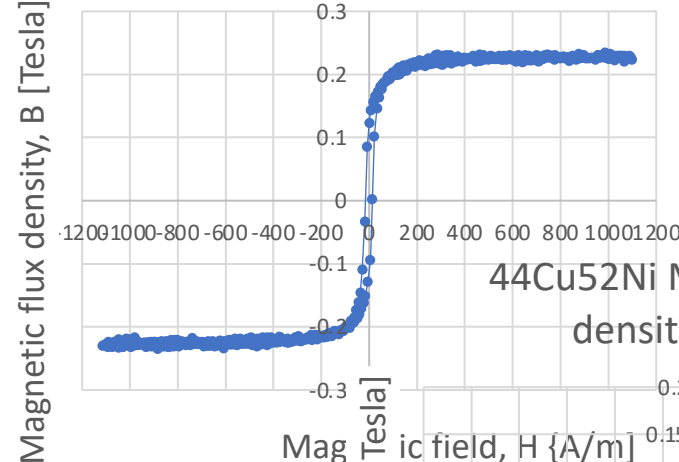
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Material results – 0Hz coercivity detail

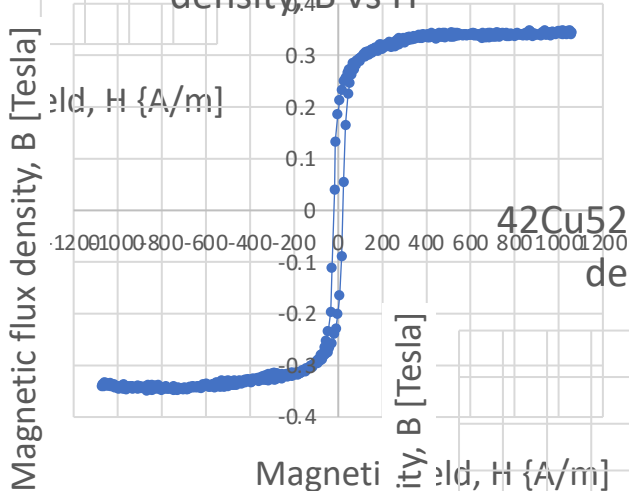
42Cu50Ni Magnetic flux density, B vs H



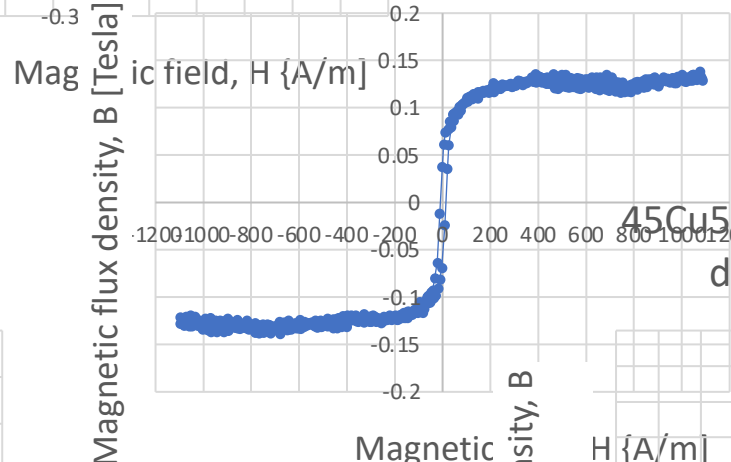
43Cu52Ni Magnetic flux density, B vs H



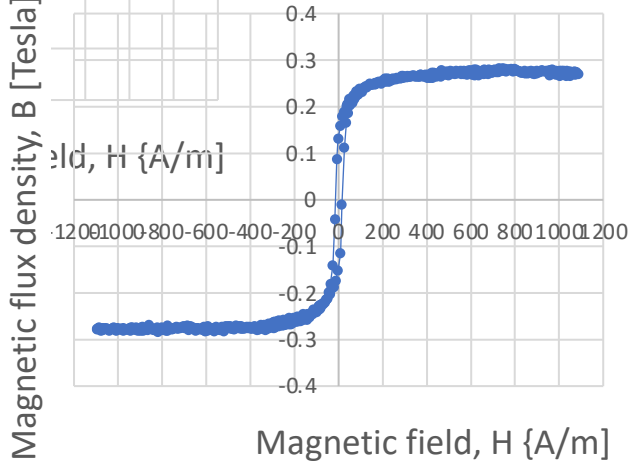
42Cu51Ni Magnetic flux density, B vs H



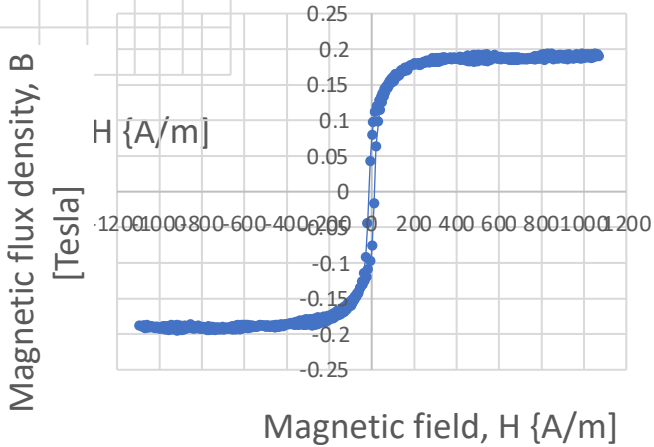
44Cu52Ni Magnetic flux density, B vs H



42Cu52Ni Magnetic flux density, B vs H

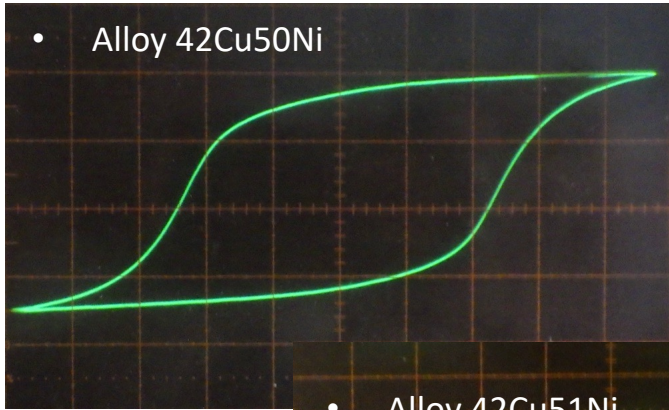


45Cu50Ni Magnetic flux density, B vs H

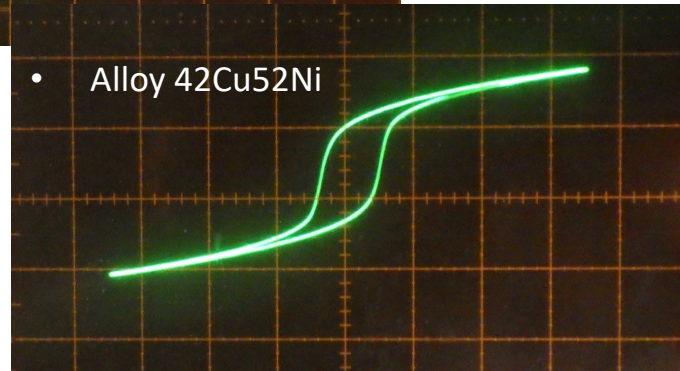
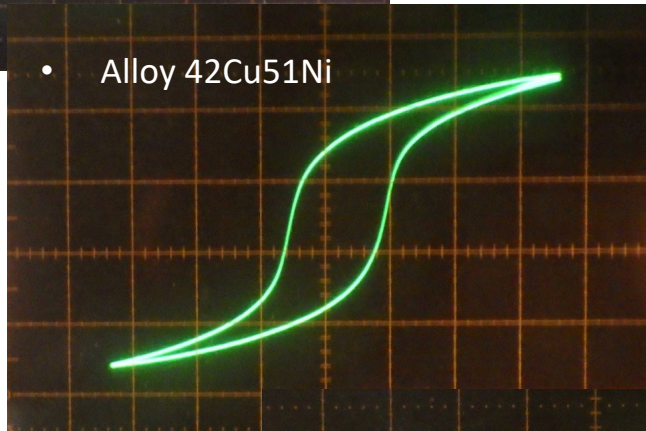


Note:
Common horizontal
scale, but differing
vertical scales

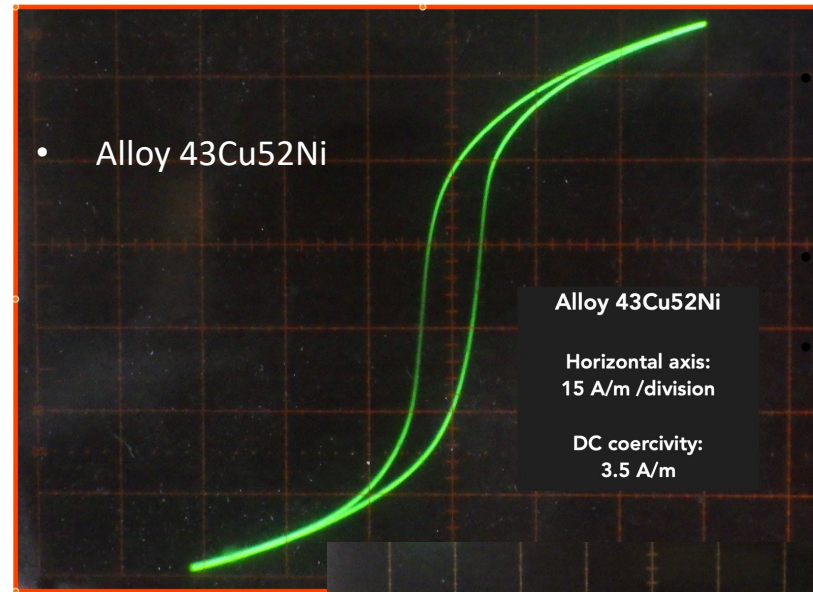
0Hz coercivity detail



All 200mT/div



15 A/m/div

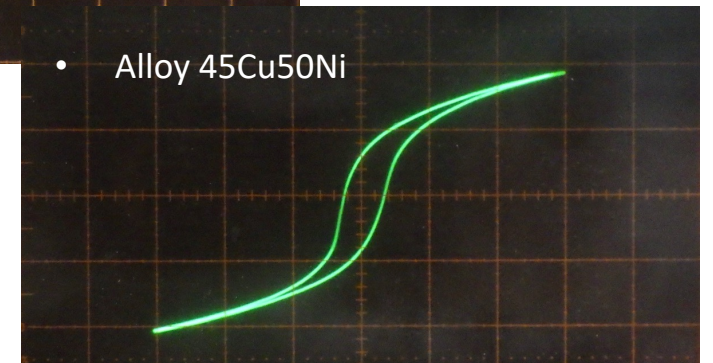


- Magnetic parameters of 43Cu52Ni are competitive with the best amorphous materials, e.g. VAC 6025

- Advantage: thicker foils

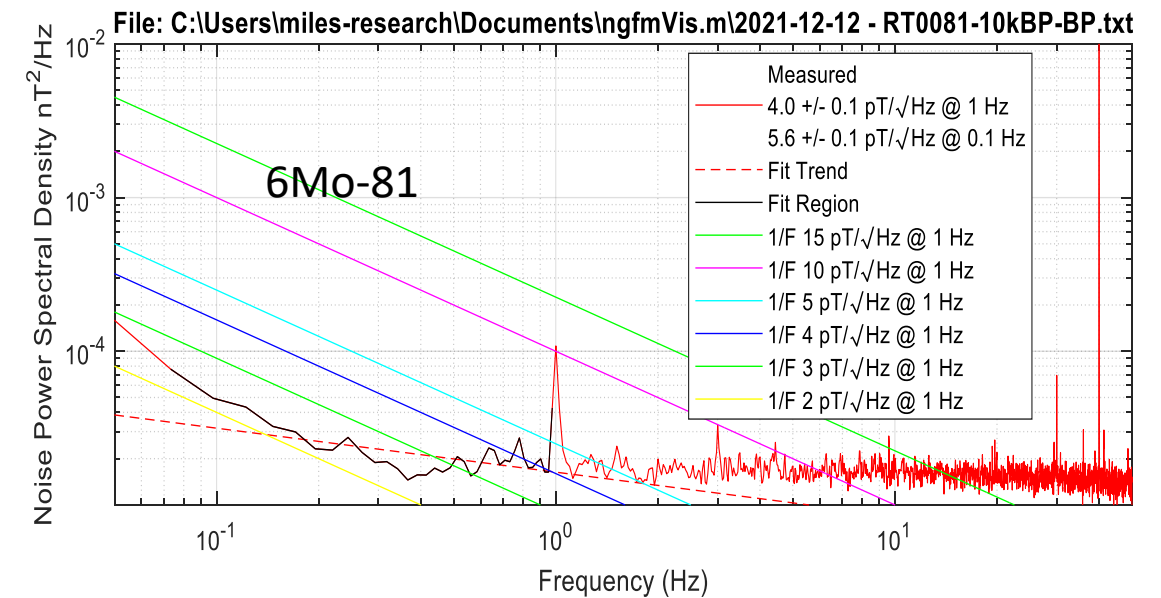
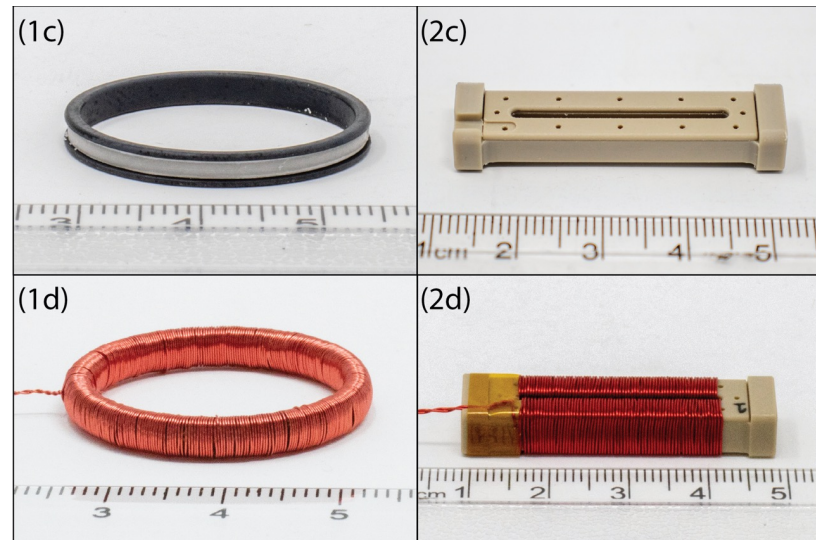


All 100mT/div



Fluxgate performance: Racetrack Test Cores

- Test cores manufactured in racetrack geometry
- Permalloy washers are heat-treated and then stacked with interleaved Kapton
- High repeatability and yield compared to standard 1" ring-core



David M. Miles and others,
Geosci. Instrum. Method. Data Syst., 11, 111–126, 2022
<https://doi.org/10.5194/gi-11-111-2022>

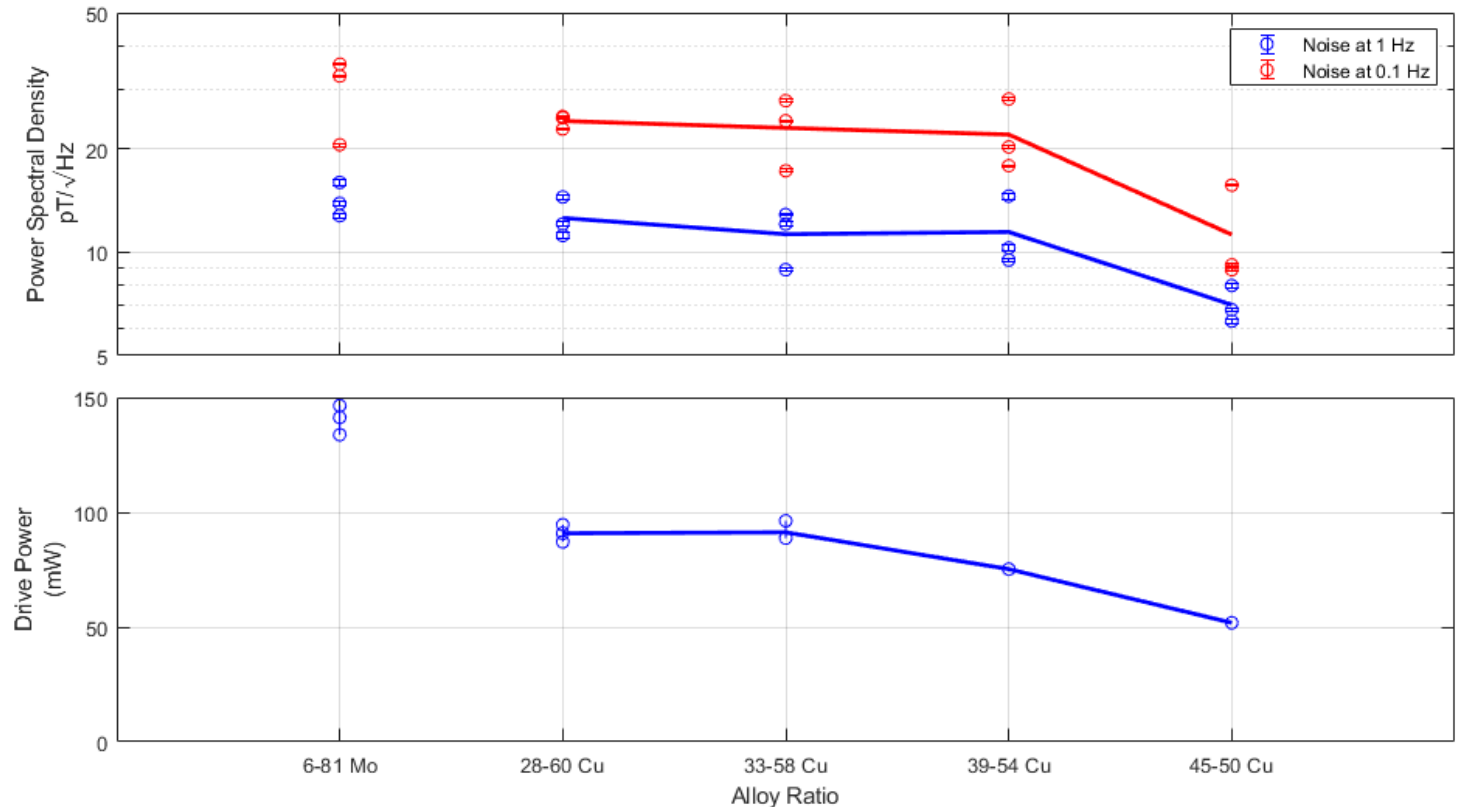
Fluxgate performance - Fluxgate Power/Noise

Experiment:

- Alloy sweep from 28 to 45% Cu
- 6-81 Mo used as a control
- All cores used 3 layers of permalloy
- QTY 3 cores for each alloy

Results:

- Noise in Power Spectral Density improves at all frequencies as %Cu increases
- Power consumption generally decreases as %Cu increases
- Cu permalloy outperforms 6-81 Mo in all metrics.



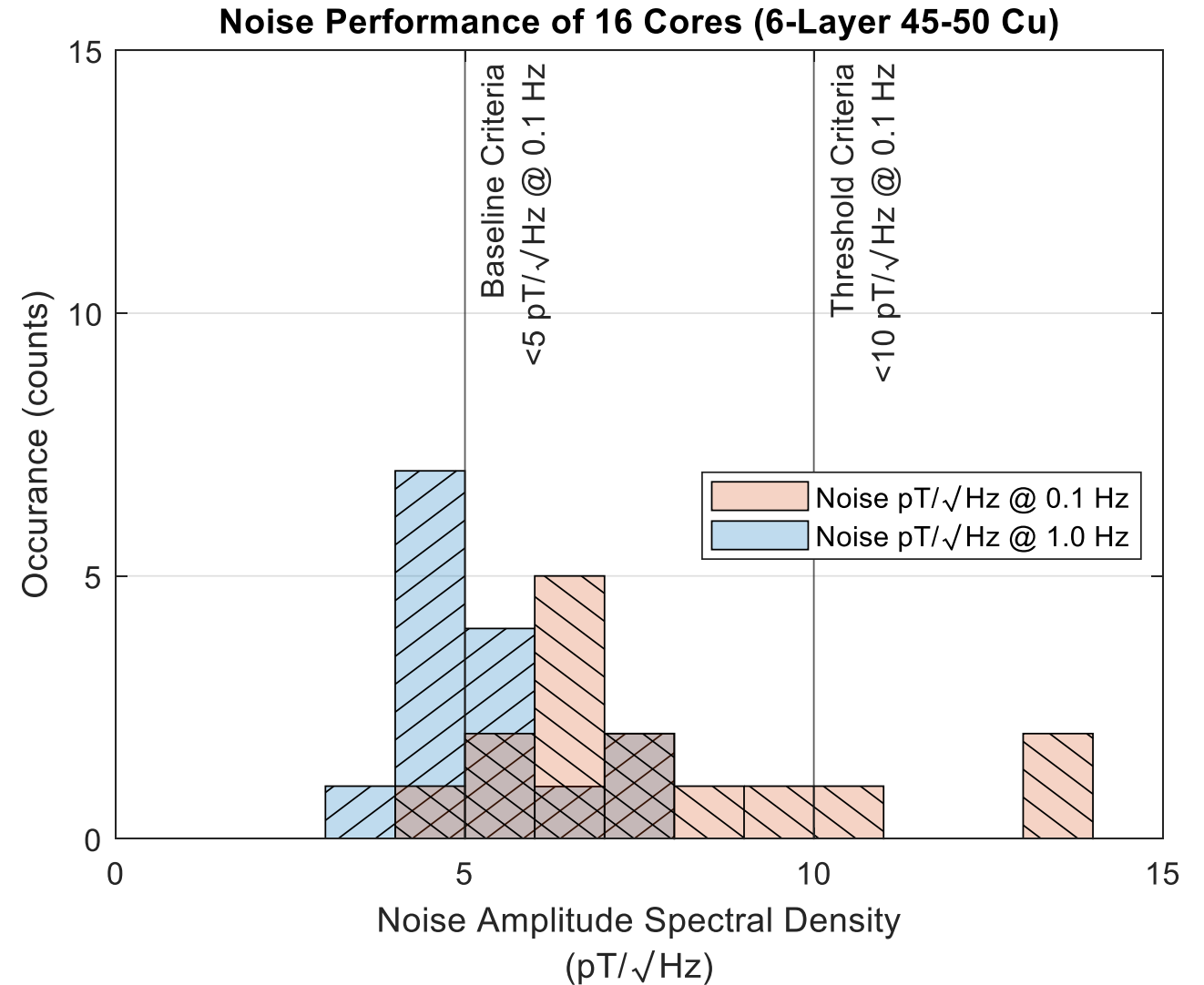
Fluxgate performance - Fluxgate Power/Noise

Experiment:

- Detail study of 45%Cu50%Ni
- 6-81 Mo used as a control
- All cores used 6 layers of permalloy

Results:

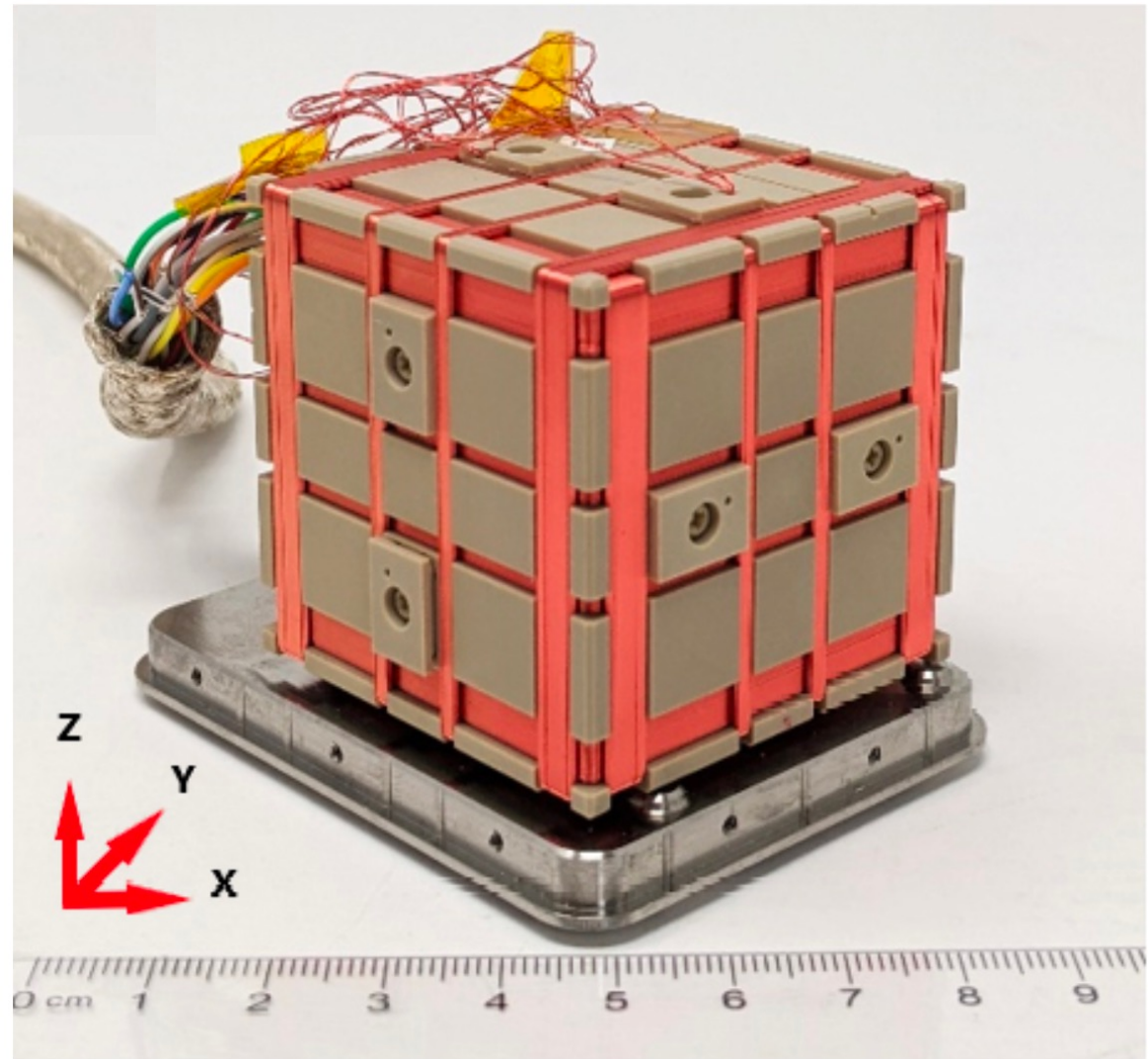
- Noise in Power Spectral Density [PSD] at 1Hz is 5 pT/rtHz [most likely]
- Noise PSD at 0.1 Hz is 8 pT/rtHz [most likely]
- Typical performance is well within INTERMAGNET 1 second standard



Tesseract sensor design

- 3 axis symmetric sensor design incorporating six racetrack cores
- 50 x 50 x 50 mm cube
- Merritt style feedback coil, requiring about 30 mW power
- Two racetrack cores per axis with an expected 3 dB further noise improvement with six cores

- Nov 20, 2022, two sensors flew successfully on ACES-II sounding rocket, reaching 188 km altitude.



Kenton Greene and others,
Geosci. Instrum. Method. Data Syst., 11, 307–321, 2022
<https://doi.org/10.5194/gi-11-307-2022>

Summary

- Copper permalloy compares favorably to traditional 6-81 Mo in noise and power consumption for use in fluxgate magnetometers
- Potential for future optimization within the Molybdenum alloy range
- Current work enables cores that meet the recent INTERMAGNET requirement <10 pT/ $\sqrt{\text{Hz}}$ @ 0.1 Hz and further improvements are likely

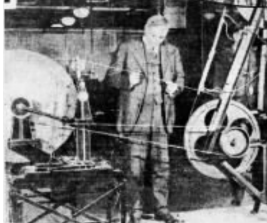
This work is funded in part by:

- MAGnetometers for Innovation and Capability (MAGIC) Technical Demonstration
80GSFC18C0008
- CHIMERA: A hybrid search coil and fluxgate magnetometer for small spacecraft missions
18-HTIDS18_2-0010

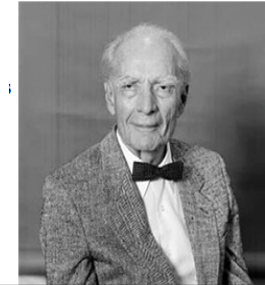
History of permalloys: Why were Cu permalloys forgotten?

- In the USA the first Permalloys were invented by G. Elmen. These included 4% Moly' Permalloy.
- Parallel developments occurred in the UK and in Germany
- By 1937 all work on Copper alloys had stopped.
- By 1969 all work on Moly' alloys for fluxgates had also stopped. 6% Moly' alloys became the preferred material.

USA [BELL LABS, NOL]



GUSTAV ELMEN, 1930
4% molybdenum permalloy

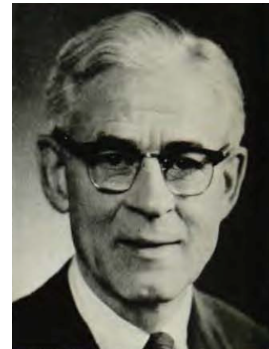


VICTOR VACQUIER, 1941
Gulf magnetometer

EUROPE [SIEMENS & HALSKE]



GEORG KEINATH, 1932
Cr & Mo molybdenum permalloy



RICHARD BOZORTH, 1947
5% molybdenum permalloy

OTTO v AUWERS & HANS NEUMANN, 1935
14% copper permalloy

1937, FULL STOP

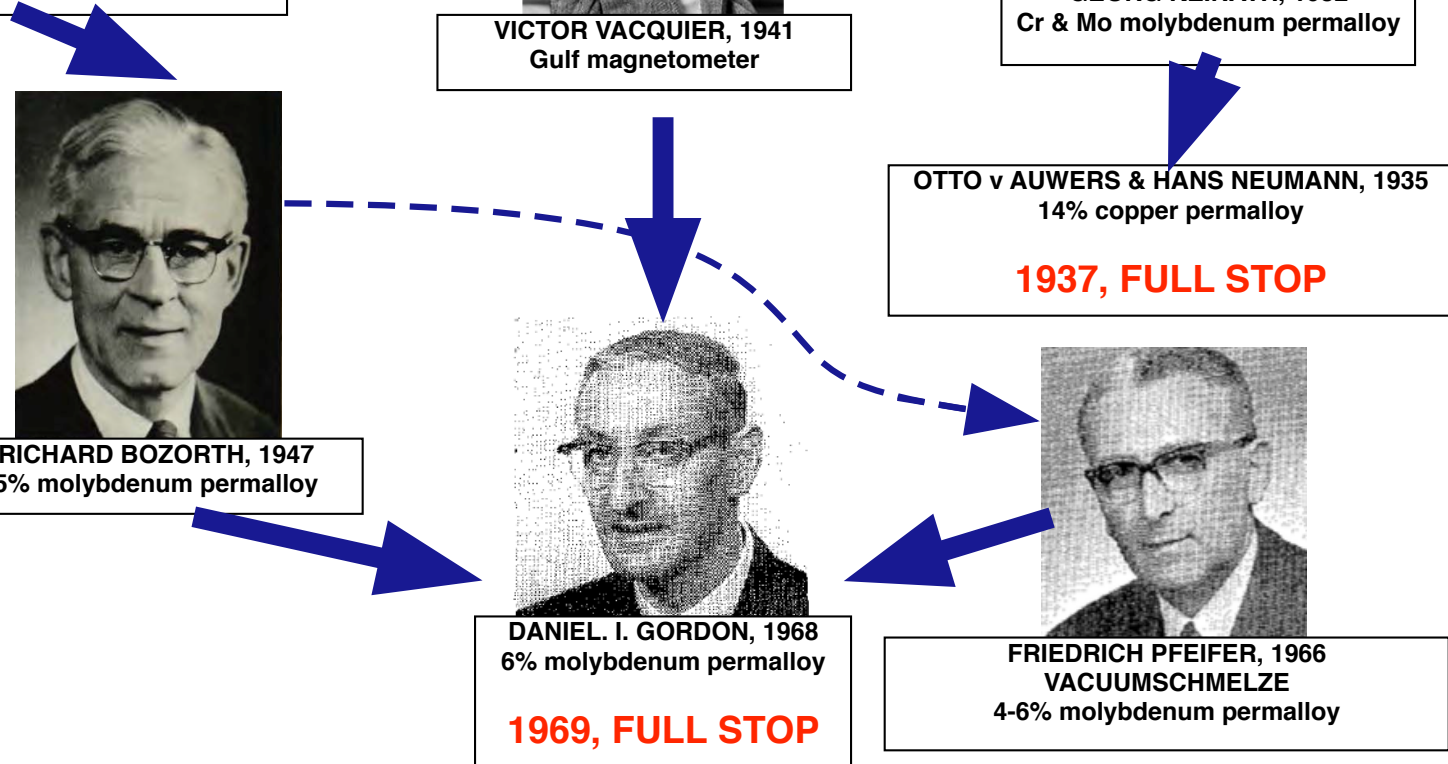


DANIEL I. GORDON, 1968
6% molybdenum permalloy



FRIEDRICH PFEIFER, 1966
VACUUMSCHMELZE
4-6% molybdenum permalloy

1969, FULL STOP



Patented June 1, 1926.

1,586,884

June 1, 1926.

1,586,884

G. W. ELMEN
MAGNETIC MATERIAL
Filed May 31, 1921

2 Sheets-Sheet 1

UNITED STATES PATENT OFFICE.

GUSTAF W. ELMEN, OF LEONIA, NEW JERSEY, ASSIGNOR TO WESTERN ELECTRIC COMPANY, INCORPORATED OF NEW YORK, N. Y., A CORPORATION OF NEW YORK.

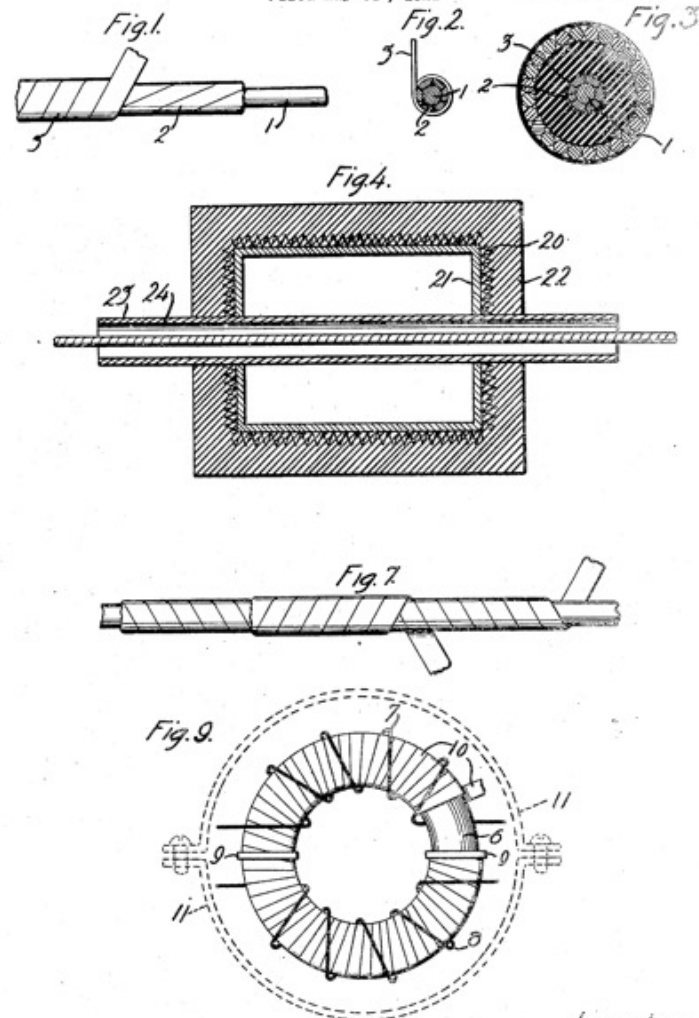
MAGNETIC MATERIAL.

Application filed May 31, 1921. Serial No. 473,877.

This invention relates to the production and use of a new material or substance having certain desirable magnetic qualities, among which are high magnetic permeability, especially at low magnetizing forces, and low hysteresis loss. It is one object of this invention to provide a suitable loading material for signaling conductors to increase their range and speed of operation. Another object relates to applying this loading material to a conductive core in a manner to produce a highly efficient transmission line for long range, high speed signaling. These objects and other objects will become apparent on consideration of examples of practice thereunder which will be disclosed specifically in this specification, with the understanding that the definition of the invention will be given in the appended claims.

This application is in part a continuation of application, Serial No. 111,080, filed July 24, 1916.

Silicon steel exhibits magnetic qualities superior to ordinary iron in some respects, but its employment is limited by its comparative brittleness and the difficulty of working it. A good quality of soft iron has been commonly employed as the best magnetic medium for general use for tractive electromagnets. The principal possible rivals of iron, nickel and cobalt, are far below it in permeability at the magnetizing forces involved in such apparatus. With nickel and cobalt, in this respect, stands Heusler's alloy of aluminum, manganese, and copper. It has been found that a composition of about $\frac{2}{3}$ nickel and $\frac{1}{3}$ copper, when tested at low magnetizing forces, gives a permeability higher than that of iron alone. It will be seen that with the exception of aluminum, all these metals stand close together in their atomic weights and atomic numbers and in this specification the five elements, manganese, iron, cobalt, nickel and copper, having the consecutive atomic numbers 25, 26, 27, 28, and 29 will be



Inventor:
Gustaf W. Elmen,
by Joel H. Palmer, Att'y

UNITED STATES PATENT OFFICE.

WILLOUGHBY STATHAM SMITH, OF BENCHAMS, NEWTON POPPLEFORD, AND HENRY JOSEPH GARNETT, OF SEVEN OAKS, ENGLAND.

MAGNETIC ALLOY.

No Drawing. Original application filed January 10, 1924, Serial No. 685,432. Divided and this application filed May 2, 1925. Serial No. 27,593.

To all whom it may concern:

Be it known that we, WILLOUGHBY STATHAM SMITH, a subject of the King of Great Britain, residing at Benchams, Newton Poppleford, Devonshire, England, and HENRY JOSEPH GARNETT, a subject of the King of Great Britain, residing at Lymne, Solefields, Seven Oaks, Kent, England, have invented a new and useful Improvement in Magnetic Alloys, of which the following is a specification.

This application is a division of our application Ser. No. 685,432, filed January 10, 1924.

This invention relates to the production of alloys possessing a high magnetic permeability especially at low magnetizing forces.

It is well known that it is desirable to add inductance to telegraphic and telephonic cables and this has before been done by wrapping around the core of the cable an iron tape or wire.

Many research workers have been investigating the properties of various alloys, especially those of nickel and iron, with a view to discovering an alloy that should be

We also preferably include a small amount of manganese to render the alloy more easy to forge.

The following are examples of alloys made in accordance with our invention

No. 1.

An alloy consisting of:—

	Per cent.
Nickel -----	74.0
Iron -----	20.0
Copper -----	5.3
Manganese -----	0.7

has an initial magnetic permeability of 7000.

No. 2.

An alloy consisting of:—

	Per cent.
Nickel -----	73.0
Copper -----	5.4
Iron -----	20.7
Tungsten -----	0.6
Manganese -----	0.3

has an electrical resistance of 25 microhms per cubic centimetre and an initial magnetic permeability of 6600.

55

65

70

75

T 173

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GEORG KEINATH, 1932

Cr & Mo molybdenum permalloy

Mißhandlung vermindert. Allen diesen ternären Legierungen ist eigen, daß ihr Sättigungswert niedriger liegt.

Eine Anzahl (Mumetall, die Nickel-Eisen-Manganlegierungen nach Gumlich) sind bereits in Z 913-1 erwähnt worden. Neue Ergebnisse liegen von Elmen⁶ vor über die Eigenschaften von Permalloy, bei dem ein Teil des Eisens (normal 21,5%) durch Chrom oder

der Temperatur. Ohne Molybdänzusatz liegt der Curiepunkt, wo das Material unmagnetisch wird, bei 580° C, nachdem vorher bei etwa 450° C ein starkes Anwachsen der Permeabilität stattfand. Für 10% Mo liegt der

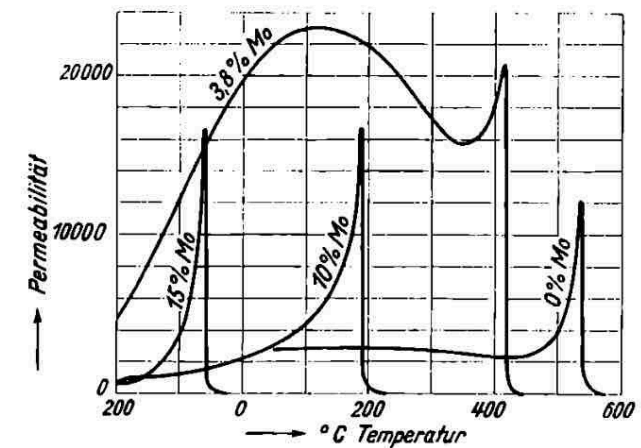


Bild 6. Permeabilität von Mo-Permalloy in Abhängigkeit von der Temperatur.

Neue magnetische Legierung „1040“ mit hoher Anfangs-Permeabilität

Z
913-5

Verfasser: Dr. Hans Neumann, Berlin-Siemensstadt

DK 681.2.03
669.144.24.018.58

Im folgenden werden ausführliche Angaben über eine neue hochpermeable Eisen-Nickel-Kupfer-Molybdän-Legierung von Siemens & Halske (Nr. 1040) mitgeteilt. Diese Legierung, die z. Z. die höchsten Werte der Anfangspermeabilität ($\mu_0 \dots 40000$) besitzt, hat zwar eine gewisse Ähnlichkeit mit dem Mu-Metall (ATM Z 913-2), unterscheidet sich aber von ihm durch ihren niedrigeren Nickelgehalt, den Zusatz von Molybdän und den dreifach höheren Kupfergehalt. Dieser ist so hoch (14%), daß hohe Werte der Anfangspermeabilität nach den bisherigen Erfahrungen dabei nicht mehr zu erwarten waren. „1040“ besteht aus etwa 72% Ni, 11% Fe, 14% Cu, 3% Mo und ist gut walzbar; das spez. Gewicht ist 8,76, der spez. Widerstand 0,56. Die in den Bildern 1...10 gegebenen magnetischen Werte wurden an 0,35 mm starken Ringen von 60 mm Außen-

und 45 mm Innendurchmesser gemessen. Gegenüber den höchsten magnetischen Werten des Mu-Metalls, der bisher besten Legierung für kleine Induktionen, wurden Anfangspermeabilität, Koerzitivkraft und Hysteresisverluste um den Faktor 2...3 verbessert. Die hohe Anfangspermeabilität der Legierung hängt zusammen mit ihrer niedrigen Magnetostriktion, die um eine Größenordnung tiefer liegt als beim Permalloy und etwa 5×10^{-7} beträgt. Die Hysteresisverluste (Bild 4) sind so gering, daß sie bei 0,35 mm Blech nur 25% der Gesamtverluste ausmachen, wie aus der für die Wirbelstromverluste typischen elliptischen Schleifenform (Bild 5) hervorgeht.

Die Alterungsbeständigkeit ist sehr hoch, eine 600 stündige Erwärmung auf 100°C hat keinen nachweisbaren Einfluß auf die magnetischen Werte.

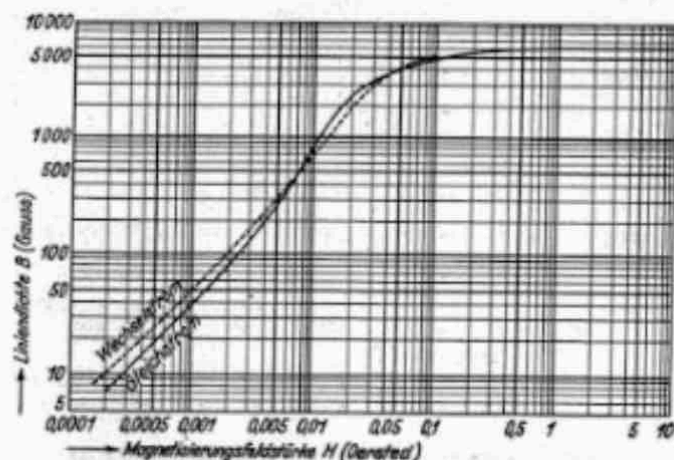


Bild 1. Magnetisierung für Gleichstrom, ballistisch gemessen, und für 50 Hz (bei vorwiegend sinusförmiger Spannung) mit dem Mu-Metall.

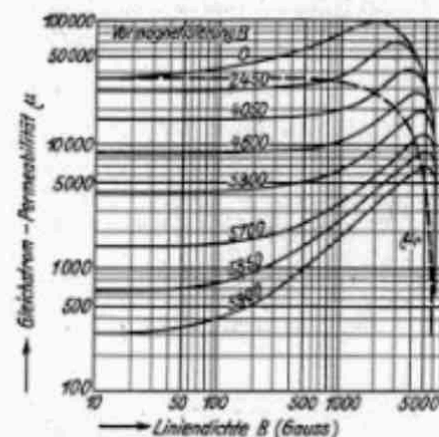
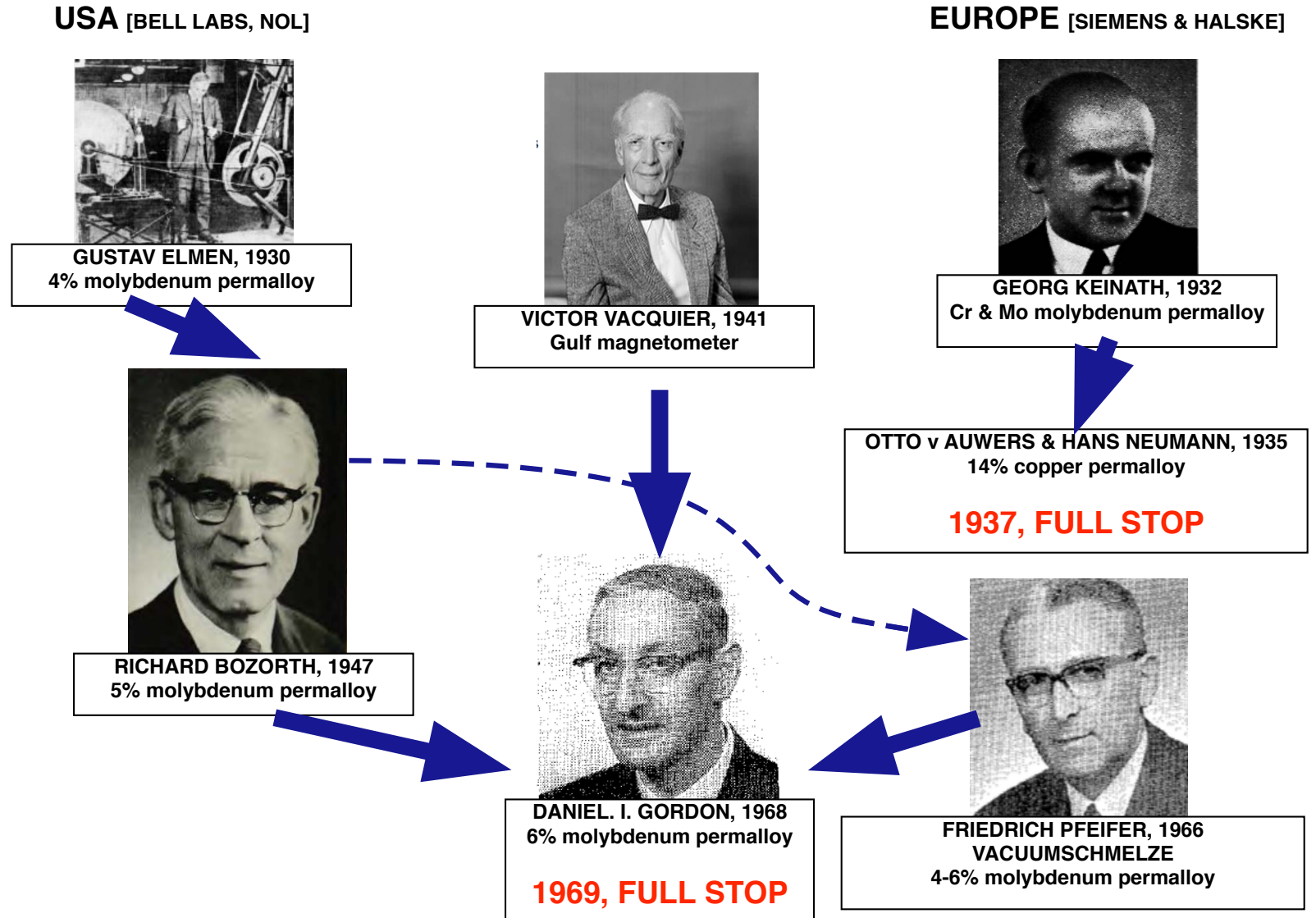


Bild 3. Gleichstrom-Permeabilität als Funktion der Induktion und reversibler Permeabilität bei verschiedenen Dauermagnetisierungen.

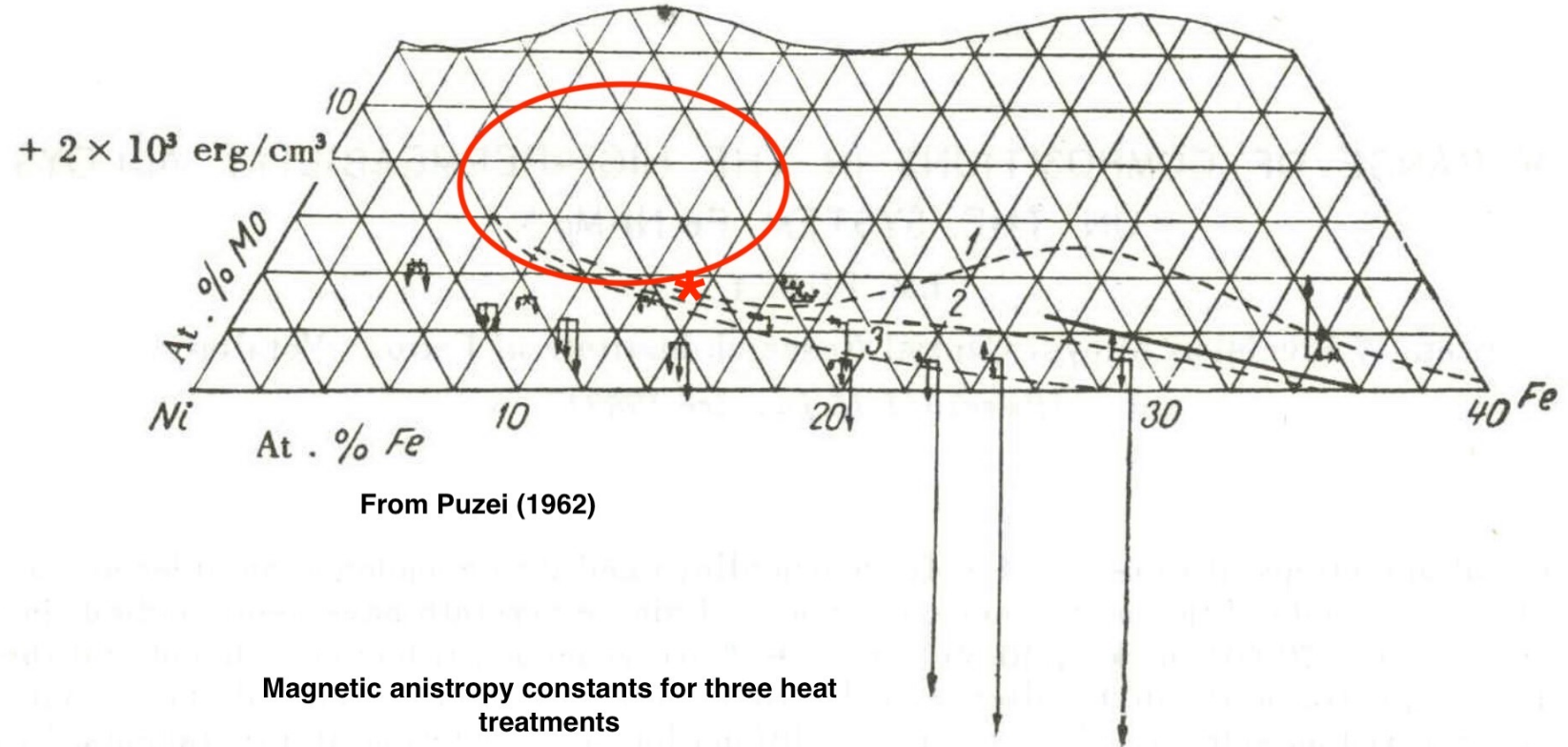
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Future work – Moly permalloys

- Additional historical examinations have found that Moly' permalloys lack a similar study of high Mo content alloys, a deficit which we intend to correct.
- The red oval indicates our expected region of interest.
- The red star locates the well known 6%Mo permalloy composition.



I.M. Puzey, 1962, A New Range of Compositions in the High-permeability Alloys on the System Fe-Ni-Mo. Fiz. Metal. Metalloved., 14, No. 3, 347-377